Crystal Structure Data

data_gkt013

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loop_

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CrysAlis RED, Oxford Diffraction Ltd.,
Version 1.171.29.9 (release 23-03-2006 CrysAlis171 .NET)
(compiled Mar 23 2006,23:39:28)
Empirical absorption correction using spherical harmonics,
implemented in SCALE3 ABSPACK scaling algorithm.
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Refinement of F^2^ against ALL reflections. The weighted R-factor wR and goodness of fit S are based on F^2^, conventional R-factors R are based on F, with F set to zero for negative F^2^. The threshold expression of $F^2^> 2sigma(F^2^)$ is used only for calculating R-factors(gt) etc. and is not relevant to the choice of reflections for refinement. R-factors based on F^2^ are statistically about twice as large as those based on F, and Rfactors based on ALL data will be even larger. _refine_ls_structure_factor_coef Fsqd

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'Flack H D (1983), Acta Cryst. A39, 876-881'

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loop_

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O2 O 0.7521(8) 0.4472(3) 0.54286(10) 0.0945(15) Uani 1 1 d . . .

O3 O 0.0943(6) 0.27867(19) 0.70860(7) 0.0478(8) Uani 1 1 d . . .

O4 O -0.0592(6) 0.6526(2) 0.72897(8) 0.0478(8) Uani 1 1 d . . .

O5 O 0.3393(7) 0.2642(3) 0.98909(8) 0.0570(11) Uani 1 1 d . . .

N1 N 0.0200(6) 0.3606(2) 0.65795(8) 0.0339(8) Uani 1 1 d . . .

C1 C 0.6880(12) 0.1702(4) 0.52137(13) 0.084(2) Uani 1 1 d . . .

H1A H 0.7232 0.1341 0.5422 0.126 Uiso 1 1 calc R . .

H1B H 0.8004 0.1543 0.5033 0.126 Uiso 1 1 calc R . .

H1C H 0.5302 0.1551 0.5135 0.126 Uiso 1 1 calc R . .

C2 C 0.7835(14) 0.5397(5) 0.54602(17) 0.114(3) Uani 1 1 d . . .

H2A H 0.6387 0.5723 0.5401 0.171 Uiso 1 1 calc R . .

H2B H 0.9081 0.5600 0.5305 0.171 Uiso 1 1 calc R . .

H2C H 0.8266 0.5545 0.5698 0.171 Uiso 1 1 calc R . .

C3 C 0.5579(9) 0.3055(3) 0.55483(11) 0.0493(13) Uani 1 1 d . . .

C4 C 0.5816(9) 0.4019(4) 0.56234(10) 0.0528(13) Uani 1 1 d . . .

C5 C 0.4450(8) 0.4420(3) 0.58859(10) 0.0459(12) Uani 1 1 d . . .

H5 H 0.4631 0.5066 0.5937 0.055 Uiso 1 1 calc R . .

C6 C 0.2807(7) 0.3886(3) 0.60774(9) 0.0337(10) Uani 1 1 d . . .

C7 C 0.1318(8) 0.4342(3) 0.63651(9) 0.0334(10) Uani 1 1 d . . .

H7 H 0.0079 0.4738 0.6258 0.040 Uiso 1 1 calc R . .

C8 C -0.1034(8) 0.2849(3) 0.63976(10) 0.0439(11) Uani 1 1 d . . .

H8A H -0.2251 0.3116 0.6246 0.053 Uiso 1 1 calc R . . H8B H -0.1797 0.2428 0.6566 0.053 Uiso 1 1 calc R . . C9 C 0.0764(8) 0.2296(3) 0.61809(11) 0.0474(12) Uani 1 d . . . H9A H 0.1634 0.1867 0.6334 0.057 Uiso 1 1 calc R . . H9B H -0.0076 0.1911 0.6009 0.057 Uiso 1 1 calc R . . C10 C 0.2503(8) 0.2933(3) 0.59932(10) 0.0380(10) Uani 1 1 d . . . C11 C 0.3901(8) 0.2532(3) 0.57265(10) 0.0432(12) Uani 1 1 d . . . H11 H 0.3685 0.1894 0.5668 0.052 Uiso 1 1 calc R ... C12 C 0.1413(8) 0.3437(3) 0.68826(9) 0.0328(10) Uani 1 1 d . . . C13 C 0.3414(7) 0.4151(3) 0.69077(9) 0.0300(10) Uani 1 1 d . . . H13 H 0.4852 0.3851 0.6813 0.036 Uiso 1 1 calc R . . C14 C 0.2618(7) 0.4928(3) 0.66486(9) 0.0319(10) Uani 1 1 d . . . H14 H 0.3996 0.5258 0.6549 0.038 Uiso 1 1 calc R . . C15 C 0.0880(8) 0.5645(3) 0.68156(9) 0.0351(10) Uani 1 1 d . . . H15A H 0.0809 0.6204 0.6666 0.042 Uiso 1 1 calc R . . H15B H -0.0692 0.5359 0.6816 0.042 Uiso 1 1 calc R . . C16 C 0.1437(7) 0.5977(3) 0.71895(9) 0.0312(9) Uani 1 1 d . . . H16 H 0.2858 0.6382 0.7189 0.037 Uiso 1 1 calc R . . C17 C 0.1860(7) 0.5105(3) 0.74152(9) 0.0251(9) Uani 1 1 d . . . H17 H 0.0460 0.4693 0.7392 0.030 Uiso 1 1 calc R . . C18 C 0.4010(7) 0.4551(3) 0.72663(9) 0.0257(9) Uani 1 1 d . . . H18 H 0.5286 0.5018 0.7231 0.031 Uiso 1 1 calc R . . C19 C 0.2466(6) 0.5173(3) 0.78098(9) 0.0228(8) Uani 1 1 d . . . C20 C 0.4395(7) 0.5931(3) 0.78673(9) 0.0330(10) Uani 1 1 d . . . H20A H 0.3726 0.6554 0.7833 0.049 Uiso 1 1 calc R . . H20B H 0.5665 0.5832 0.7703 0.049 Uiso 1 1 calc R . . H20C H 0.5002 0.5881 0.8102 0.049 Uiso 1 1 calc R ... C21 C 0.0384(7) 0.5349(3) 0.80563(8) 0.0270(9) Uani 1 1 d . . . H21A H -0.0913 0.4922 0.7997 0.032 Uiso 1 1 calc R . . H21B H -0.0175 0.6000 0.8029 0.032 Uiso 1 1 calc R . . C22 C 0.1134(7) 0.5182(3) 0.84389(8) 0.0273(9) Uani 1 1 d . . .

H22A H 0.2249 0.5678 0.8506 0.033 Uiso 1 1 calc R . . H22B H -0.0258 0.5246 0.8588 0.033 Uiso 1 1 calc R . . C23 C 0.2274(6) 0.4216(3) 0.85096(8) 0.0230(8) Uani 1 1 d . . . H23 H 0.1011 0.3740 0.8482 0.028 Uiso 1 1 calc R . . C24 C 0.4220(7) 0.3952(3) 0.82439(9) 0.0246(8) Uani 1 1 d . . . H24 H 0.5609 0.4359 0.8286 0.030 Uiso 1 1 calc R . . C25 C 0.3296(6) 0.4143(3) 0.78730(8) 0.0251(9) Uani 1 1 d . . . H25 H 0.1860 0.3752 0.7851 0.030 Uiso 1 1 calc R . . C26 C 0.4859(7) 0.3866(3) 0.75581(9) 0.0313(10) Uani 1 1 d . . . H26A H 0.4606 0.3205 0.7492 0.038 Uiso 1 1 calc R . . H26B H 0.6532 0.3961 0.7610 0.038 Uiso 1 1 calc R . . C27 C 0.3182(6) 0.4121(3) 0.88949(9) 0.0248(9) Uani 1 1 d . . . C28 C 0.4862(7) 0.4949(3) 0.89925(10) 0.0354(10) Uani 1 1 d . . . H28A H 0.5577 0.4823 0.9217 0.053 Uiso 1 1 calc R . . H28B H 0.3972 0.5533 0.9004 0.053 Uiso 1 1 calc R . . H28C H 0.6082 0.5006 0.8818 0.053 Uiso 1 1 calc R . . C29 C 0.1013(7) 0.4137(3) 0.91453(9) 0.0347(10) Uani 1 1 d . . . H29A H 0.0316 0.4771 0.9142 0.042 Uiso 1 1 calc R . . H29B H -0.0174 0.3694 0.9059 0.042 Uiso 1 1 calc R . . C30 C 0.1624(7) 0.3876(3) 0.95257(10) 0.0396(11) Uani 1 1 d . . . H30A H 0.2717 0.4343 0.9622 0.047 Uiso 1 1 calc R . . H30B H 0.0189 0.3881 0.9667 0.047 Uiso 1 1 calc R . . C31 C 0.2740(8) 0.2903(3) 0.95378(9) 0.0396(11) Uani 1 1 d . . . H31 H 0.1603 0.2433 0.9447 0.047 Uiso 1 1 calc R . . C32 C 0.4968(8) 0.2876(3) 0.93156(9) 0.0395(11) Uani 1 d . . . H32A H 0.5605 0.2232 0.9315 0.047 Uiso 1 1 calc R . . H32B H 0.6155 0.3294 0.9418 0.047 Uiso 1 1 calc R . . C33 C 0.4486(7) 0.3184(3) 0.89408(10) 0.0322(10) Uani 1 1 d . . . C34 C 0.5221(8) 0.2658(3) 0.86752(10) 0.0393(11) Uani 1 1 d . . . H34 H 0.5963 0.2082 0.8728 0.047 Uiso 1 1 calc R . . C35 C 0.4951(8) 0.2916(3) 0.82935(9) 0.0381(11) Uani 1 1 d . . .

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C13 0.034(2) 0.032(2) 0.0240(19) -0.0004(17) 0.0037(18) 0.007(2) C14 0.039(2) 0.034(2) 0.0232(18) 0.0009(17) 0.0038(19) -0.003(2) C15 0.051(3) 0.031(2) 0.024(2) 0.0057(16) -0.002(2) -0.007(2) C16 0.038(2) 0.026(2) 0.030(2) 0.0010(17) 0.0001(19) 0.002(2) C17 0.026(2) 0.020(2) 0.0291(19) -0.0003(16) -0.0046(18) -0.0057(18) C18 0.025(2) 0.026(2) 0.0258(19) 0.0012(16) 0.0050(18) -0.0026(19) C19 0.0208(19) 0.025(2) 0.0228(18) -0.0003(15) -0.0012(17) 0.0035(18) C20 0.034(2) 0.032(2) 0.033(2) 0.0021(18) -0.0019(19) 0.003(2) C21 0.026(2) 0.024(2) 0.031(2) 0.0012(16) 0.0019(18) 0.0031(19) C22 0.026(2) 0.033(2) 0.0228(19) -0.0007(16) 0.0078(18) 0.003(2) C23 0.0212(19) 0.022(2) 0.0257(18) 0.0016(15) 0.0014(16) -0.0052(18) C24 0.025(2) 0.023(2) 0.0260(19) 0.0014(16) 0.0012(17) -0.0031(18) C25 0.024(2) 0.029(2) 0.0221(18) -0.0009(16) -0.0001(17) 0.0034(18) C26 0.034(2) 0.032(2) 0.027(2) 0.0020(17) 0.0012(19) 0.009(2) C27 0.024(2) 0.028(2) 0.0229(19) -0.0001(16) 0.0014(16) 0.0071(18) C28 0.036(2) 0.035(3) 0.035(2) -0.0003(18) 0.002(2) 0.004(2) C29 0.029(2) 0.044(3) 0.031(2) 0.0045(19) 0.0030(19) 0.005(2) C30 0.033(2) 0.055(3) 0.030(2) 0.009(2) 0.006(2) 0.000(2) C31 0.045(3) 0.048(3) 0.025(2) 0.0115(19) 0.000(2) -0.004(2) C32 0.041(3) 0.043(3) 0.034(2) 0.0078(19) 0.001(2) 0.010(2) C33 0.031(2) 0.039(3) 0.027(2) 0.0011(18) 0.000(2) 0.001(2) C34 0.053(3) 0.025(2) 0.040(2) 0.0089(19) -0.007(2) 0.013(2) C35 0.051(3) 0.036(2) 0.027(2) -0.0036(18) -0.001(2) 0.019(2)

_geom_special_details

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All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles; correlations between esds in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell esds is used for estimating esds involving l.s. planes.

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loop_

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C19 C21 1.520(5) . ?

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- C19 C25 1.536(5) . ?
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- C25 H25 0.9800 . ?
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- C30 C31 1.502(6) . ?
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- C30 H30B 0.9700 . ?
- C31 C32 1.512(5).?
- C31 H31 0.9800 . ?
- C32 C33 1.516(5) . ?
- C32 H32A 0.9700 . ?
- C32 H32B 0.9700 . ?
- C33 C34 1.318(5).?
- C34 C35 1.506(5).?
- C34 H34 0.9300 . ?
- C35 H35A 0.9700 . ?
- C35 H35B 0.9700 . ?

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_geom_angle_atom_site_label_3

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_geom_angle_site_symmetry_1

_geom_angle_site_symmetry_3

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C3 O1 C1 118.0(4) . . ?

- C2 O2 C4 120.1(5) . . ?
- C16 O4 H104 111(5) . . ?
- C31 O5 H105 95(4) . . ?
- C12 N1 C8 121.4(3) . . ?
- C12 N1 C7 112.4(3) . . ?
- C8 N1 C7 117.2(3) . . ?
- O1 C1 H1A 109.5 . . ?
- O1 C1 H1B 109.5 . . ?
- H1A C1 H1B 109.5 . . ?
- O1 C1 H1C 109.5 . . ?

H1A C1 H1C 109.5 . . ? H1B C1 H1C 109.5 . . ? O2 C2 H2A 109.5 . . ? O2 C2 H2B 109.5 . . ? H2A C2 H2B 109.5 . . ? O2 C2 H2C 109.5 . . ? H2A C2 H2C 109.5 . . ? H2B C2 H2C 109.5 . . ? O1 C3 C11 124.5(4) . . ? O1 C3 C4 116.6(4) . . ? C11 C3 C4 118.9(4) . . ? O2 C4 C5 126.4(4) . . ? O2 C4 C3 114.0(4) . . ? C5 C4 C3 119.5(4) . . ? C4 C5 C6 121.9(4) . . ? C4 C5 H5 119.1 . . ? C6 C5 H5 119.1 . . ? C10 C6 C5 118.6(4) . . ? C10 C6 C7 120.3(4) . . ? C5 C6 C7 121.0(4) . . ? N1 C7 C6 110.1(3) . . ? N1 C7 C14 100.9(3) . . ? C6 C7 C14 117.9(4) . . ? N1 C7 H7 109.2 . . ? C6 C7 H7 109.2 . . ? C14 C7 H7 109.2 . . ? N1 C8 C9 108.4(4) . . ? N1 C8 H8A 110.0 . . ? C9 C8 H8A 110.0 . . ? N1 C8 H8B 110.0 . . ? C9 C8 H8B 110.0 . . ?

H8A C8 H8B 108.4 . . ? C10 C9 C8 112.8(4) . . ? C10 C9 H9A 109.0 . . ? C8 C9 H9A 109.0 . . ? C10 C9 H9B 109.0 . . ? C8 C9 H9B 109.0 . . ? H9A C9 H9B 107.8 . . ? C6 C10 C11 119.0(4) . . ? C6 C10 C9 122.9(4) . . ? C11 C10 C9 118.1(4) . . ? C3 C11 C10 122.0(4) . . ? C3 C11 H11 119.0 . . ? C10 C11 H11 119.0 . . ? O3 C12 N1 123.9(4) . . ? O3 C12 C13 127.9(4) . . ? N1 C12 C13 108.2(3) . . ? C12 C13 C18 117.9(3) . . ? C12 C13 C14 102.2(3) . . ? C18 C13 C14 112.5(3) . . ? C12 C13 H13 107.9 . . ? C18 C13 H13 107.9 . . ? C14 C13 H13 107.9 . . ? C13 C14 C15 112.5(3) . . ? C13 C14 C7 102.2(3) . . ? C15 C14 C7 109.6(3) . . ? C13 C14 H14 110.8 . . ? C15 C14 H14 110.8 . . ? C7 C14 H14 110.8 . . ? C16 C15 C14 117.0(3) . . ? C16 C15 H15A 108.1 . . ? C14 C15 H15A 108.1 . . ?

C16 C15 H15B 108.1 . . ?

- C14 C15 H15B 108.1 . . ?
- H15A C15 H15B 107.3 . . ?
- O4 C16 C17 114.1(3) . . ?
- O4 C16 C15 104.4(3) . . ?
- C17 C16 C15 108.3(3) . . ?
- O4 C16 H16 109.9 . . ?
- C17 C16 H16 109.9 . . ?
- C15 C16 H16 109.9 . . ?
- C16 C17 C19 122.5(3) . . ?
- C16 C17 C18 108.7(3) . . ?
- C19 C17 C18 102.5(3) . . ?
- C16 C17 H17 107.4 . . ?
- C19 C17 H17 107.4 . . ?
- C18 C17 H17 107.4 . . ?
- C13 C18 C26 119.2(3) . . ?
- C13 C18 C17 110.1(3) . . ?
- C26 C18 C17 106.9(3) . . ?
- C13 C18 H18 106.7 . . ?
- C26 C18 H18 106.7 . . ?
- C17 C18 H18 106.7 . . ?
- C21 C19 C20 110.1(3) . . ?
- C21 C19 C25 106.8(3) . . ?
- C20 C19 C25 114.4(3) . . ?
- C21 C19 C17 116.2(3) . . ?
- C20 C19 C17 109.7(3) . . ?
- C25 C19 C17 99.3(3) . . ?
- C19 C20 H20A 109.5 . . ?
- C19 C20 H20B 109.5 . . ?
- H20A C20 H20B 109.5 . . ?
- C19 C20 H20C 109.5 . . ?

H20A C20 H20C 109.5 . . ? H20B C20 H20C 109.5 . . ? C19 C21 C22 110.5(3) . . ? C19 C21 H21A 109.6 . . ? C22 C21 H21A 109.6 . . ? C19 C21 H21B 109.6 . . ? C22 C21 H21B 109.6 . . ? H21A C21 H21B 108.1 . . ? C23 C22 C21 114.8(3) . . ? C23 C22 H22A 108.6 . . ? C21 C22 H22A 108.6 . . ? C23 C22 H22B 108.6 . . ? C21 C22 H22B 108.6 . . ? H22A C22 H22B 107.6 . . ? C22 C23 C24 113.4(3) . . ? C22 C23 C27 112.3(3) . . ? C24 C23 C27 111.5(3) . . ? C22 C23 H23 106.3 . . ? C24 C23 H23 106.3 . . ? C27 C23 H23 106.3 . . ? C35 C24 C25 111.9(3) . . ? C35 C24 C23 109.9(3) . . ? C25 C24 C23 109.0(3) . . ? C35 C24 H24 108.7 . . ? C25 C24 H24 108.7 . . ? C23 C24 H24 108.7 . . ? C24 C25 C19 114.4(3) . . ? C24 C25 C26 118.8(3) . . ? C19 C25 C26 106.8(3) . . ? C24 C25 H25 105.2 . . ? C19 C25 H25 105.2 . . ?

C26 C25 H25 105.2 . . ? C25 C26 C18 103.1(3) . . ? C25 C26 H26A 111.1 . . ? C18 C26 H26A 111.1 . . ? C25 C26 H26B 111.1 . . ? C18 C26 H26B 111.1 . . ? H26A C26 H26B 109.1 . . ? C33 C27 C28 109.2(3) . . ? C33 C27 C29 108.8(3) . . ? C28 C27 C29 108.8(3) . . ? C33 C27 C23 109.9(3) . . ? C28 C27 C23 111.3(3) . . ? C29 C27 C23 108.7(3) . . ? C27 C28 H28A 109.5 . . ? C27 C28 H28B 109.5 . . ? H28A C28 H28B 109.5 . . ? C27 C28 H28C 109.5 . . ? H28A C28 H28C 109.5 . . ? H28B C28 H28C 109.5 . . ? C30 C29 C27 113.7(3) . . ? C30 C29 H29A 108.8 . . ? C27 C29 H29A 108.8 . . ? C30 C29 H29B 108.8 . . ? C27 C29 H29B 108.8 . . ? H29A C29 H29B 107.7 . . ? C31 C30 C29 109.9(3) . . ? C31 C30 H30A 109.7 . . ? C29 C30 H30A 109.7 . . ? C31 C30 H30B 109.7 . . ? C29 C30 H30B 109.7 . . ? H30A C30 H30B 108.2 . . ?

O5 C31 C30 111.4(3) . . ?

O5 C31 C32 107.7(3) . . ?

C30 C31 C32 110.6(3) . . ?

O5 C31 H31 109.0 . . ?

C30 C31 H31 109.0 . . ?

C32 C31 H31 109.0 . . ?

C31 C32 C33 111.8(3) . . ?

C31 C32 H32A 109.3 . . ?

C33 C32 H32A 109.3 . . ?

C31 C32 H32B 109.3 . . ?

C33 C32 H32B 109.3 . . ?

H32A C32 H32B 107.9 . . ?

C34 C33 C27 123.3(3) . . ?

C34 C33 C32 120.5(4) . . ?

C27 C33 C32 116.3(3) . . ?

C33 C34 C35 125.1(4) . . ?

C33 C34 H34 117.5 . . ?

C35 C34 H34 117.5 . . ?

C34 C35 C24 112.1(3) . . ?

C34 C35 H35A 109.2 . . ?

C24 C35 H35A 109.2 . . ?

C34 C35 H35B 109.2 . . ?

C24 C35 H35B 109.2 . . ?

H35A C35 H35B 107.9 . . ?

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_geom_torsion_site_symmetry_1 _geom_torsion_site_symmetry_2 _geom_torsion_site_symmetry_3 _geom_torsion_site_symmetry_4 _geom_torsion_publ_flag C1 O1 C3 C11 -3.5(7) . . . ? C1 O1 C3 C4 178.2(5) ? C2 O2 C4 C5 -6.5(9) ? C2 O2 C4 C3 176.2(6) ? O1 C3 C4 O2 -1.0(7) ? C11 C3 C4 O2 -179.4(4) ? O1 C3 C4 C5 -178.4(4) ? C11 C3 C4 C5 3.1(7) . . . ? O2 C4 C5 C6 -177.8(5) . . . ? C3 C4 C5 C6 -0.7(7) ? C4 C5 C6 C10 -1.8(6) ? C4 C5 C6 C7 -179.9(4) ? C12 N1 C7 C6 98.7(4) ? C8 N1 C7 C6 -49.1(5) ? C12 N1 C7 C14 -26.6(4) ? C8 N1 C7 C14 -174.4(3) ? C10 C6 C7 N1 15.9(5) . . . ? C5 C6 C7 N1 -166.0(4) ? C10 C6 C7 C14 130.9(4) ? C5 C6 C7 C14 -51.1(5) . . . ? C12 N1 C8 C9 -81.1(4)? C7 N1 C8 C9 63.6(5)? N1 C8 C9 C10 -42.7(5) . . . ? C5 C6 C10 C11 1.9(6) . . . ? C7 C6 C10 C11 179.9(4)? C5 C6 C10 C9 -179.4(4)?

C7 C6 C10 C9 -1.4(6) ? C8 C9 C10 C6 15.2(6) ? C8 C9 C10 C11 -166.1(4) ? O1 C3 C11 C10 178.6(4) ? C4 C3 C11 C10 -3.1(7) . . . ? C6 C10 C11 C3 0.6(6) ? C9 C10 C11 C3 -178.1(4)? C8 N1 C12 O3 -26.2(6) ? C7 N1 C12 O3 -172.4(4)? C8 N1 C12 C13 151.5(3) . . . ? C7 N1 C12 C13 5.3(4)? O3 C12 C13 C18 -40.0(6) ? N1 C12 C13 C18 142.5(3)? O3 C12 C13 C14 -163.8(4) ? N1 C12 C13 C14 18.6(4) ? C12 C13 C14 C15 83.9(4) . . . ? C18 C13 C14 C15 -43.5(4) ? C12 C13 C14 C7 -33.5(4) ? C18 C13 C14 C7 -161.0(3) ? N1 C7 C14 C13 36.1(4) ? C6 C7 C14 C13 -83.8(4) ? N1 C7 C14 C15 -83.4(3) . . . ? C6 C7 C14 C15 156.8(3) . . . ? C13 C14 C15 C16 41.7(5)? C7 C14 C15 C16 154.7(3) . . . ? C14 C15 C16 O4 -172.8(3) . . . ? C14 C15 C16 C17 -50.8(4)? O4 C16 C17 C19 -64.0(5) . . . ? C15 C16 C17 C19 -179.9(3) . . . ? O4 C16 C17 C18 176.9(3) . . . ? C15 C16 C17 C18 61.0(4) ?

C12 C13 C18 C26 61.8(5) ? C14 C13 C18 C26 -179.6(3) ? C12 C13 C18 C17 -62.1(4) ? C14 C13 C18 C17 56.4(4) ? C16 C17 C18 C13 -66.2(4) ? C19 C17 C18 C13 162.8(3) . . . ? C16 C17 C18 C26 163.0(3) . . . ? C19 C17 C18 C26 31.9(4)? C16 C17 C19 C21 79.5(4) . . . ? C18 C17 C19 C21 -158.5(3) . . . ? C16 C17 C19 C20 -46.3(5)? C18 C17 C19 C20 75.8(3) . . . ? C16 C17 C19 C25 -166.5(3) . . . ? C18 C17 C19 C25 -44.5(3) ? C20 C19 C21 C22 -66.9(4) ? C25 C19 C21 C22 57.9(4) . . . ? C17 C19 C21 C22 167.6(3) . . . ? C19 C21 C22 C23 -53.5(4) . . . ? C21 C22 C23 C24 47.8(4) ? C21 C22 C23 C27 175.3(3) . . . ? C22 C23 C24 C35 -170.0(3) . . . ? C27 C23 C24 C35 62.0(4) ? C22 C23 C24 C25 -47.1(4) . . . ? C27 C23 C24 C25 -175.0(3) . . . ? C35 C24 C25 C19 178.4(3) . . . ? C23 C24 C25 C19 56.7(4) . . . ? C35 C24 C25 C26 -53.8(5)? C23 C24 C25 C26 -175.6(3) . . . ? C21 C19 C25 C24 -62.7(4) . . . ? C20 C19 C25 C24 59.5(4) . . . ? C17 C19 C25 C24 176.2(3) . . . ?

C21 C19 C25 C26 163.7(3) . . . ? C20 C19 C25 C26 -74.2(4) ? C17 C19 C25 C26 42.6(4) ? C24 C25 C26 C18 -154.4(3) ? C19 C25 C26 C18 -23.2(4) ? C13 C18 C26 C25 -131.2(4) . . . ? C17 C18 C26 C25 -5.7(4) . . . ? C22 C23 C27 C33 -175.0(3) . . . ? C24 C23 C27 C33 -46.5(4) . . . ? C22 C23 C27 C28 -53.9(4)? C24 C23 C27 C28 74.6(4) ? C22 C23 C27 C29 65.9(4) . . . ? C24 C23 C27 C29 -165.5(3) . . . ? C33 C27 C29 C30 50.2(4) . . . ? C28 C27 C29 C30 -68.7(4) ? C23 C27 C29 C30 169.9(3) . . . ? C27 C29 C30 C31 -57.7(5) ? C29 C30 C31 O5 178.6(4) ? C29 C30 C31 C32 58.8(4) ? O5 C31 C32 C33 -177.4(4) ? C30 C31 C32 C33 -55.4(5) . . . ? C28 C27 C33 C34 -107.2(5) ? C29 C27 C33 C34 134.1(4)? C23 C27 C33 C34 15.1(5)? C28 C27 C33 C32 71.6(4) ? C29 C27 C33 C32 -47.1(4)? C23 C27 C33 C32 -166.0(3) . . . ? C31 C32 C33 C34 -130.0(4) . . . ? C31 C32 C33 C27 51.1(5) . . . ? C27 C33 C34 C35 2.0(7) . . . ? C32 C33 C34 C35 -176.8(4) . . . ? C33 C34 C35 C24 12.5(7) ? C25 C24 C35 C34 -164.4(3) ? C23 C24 C35 C34 -43.2(5) ?

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