Treatment of rice grain based biodigester distillery effluent (BDE) using inorganic coagulants

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The removal of COD and colour from biodigester effluent (BDE) of rice grain based alcohol distillery plant has been studied using inorganic coagulant such as $CaCO_3$, $CuNO_3$ and Na_2SiO_3 . $CuNO_3$ is found to be more effective, among all coagulant. COD reduction of 78, 83 and 51% and colour reduction of 75, 78 and 41% is obtained using 60 mM CaCO₃, 40 mM CuNO₃ and 40 mM Na₂SiO₃ respectively, at their optimum initial *p*H_i. The *p*H of effluent-coagulant mixture play a major role in removal of pollutant from the BDE. CuNO₃ gives 83% COD reduction and 78% colour reduction along with good settling property. 82% settling occurred with alum in 25 min. The properties of filtrate and residues have also been analyzed.

Keywords: Rice grain based biodigester effluent, Chemical oxygen demand, Settling, Coagulation, Copper nitrate

Alcohol is produced in distilleries by fermentation of sugar cane juice, sugar cane molasses, sugar beet, rice grains, etc. Demand of alcohol is increasing day by day in the field of energy and pharma sector. In India more than 70% ethanol is produced by sugar cane molasses¹ but India is the largest rice producing country in the world, therefore it may be used as a major supplementary raw material for distillery industries at the place of molasses.

Ethanol is produced by fermentation of raw material in fermentation broth. The fermentation broth containing 6-10% alcohol by volume is distilled to recover alcohol remaining is the waste called spent wash (SW). The characteristic of SW depends on raw material and process being used by the industries. For example, effluent from the sugar cane molasses based distilleries have very high COD (i.e. 90000-150000 mg/dm³)², on the other hand SW from timothy grass based distillery contains COD 26000-50000 mg/dm³ reported by Belkacemi *et al.*³ Grapes based distillery units SW have COD 22000-48000 mg/dm³ reported by Wolmarans *et al.*⁴.

The rice grain based SW also contains high COD (35,000-50,000) mg/dm³ and BOD (7000-10,000) mg/dm³, and it is sent to the biodigester for anaerobic treatment. Biodigester can reduce 60 to 75 percent COD and 65 to 80% BOD from the spent wash.

The output of biodigester called BDE is dark brown in colour, due to the presence of melanoidin and other compound like proteins, waxes and carbohydrates, etc which contributes to COD (10,000-14,000) mg/dm³ and BOD (1,500-3,000) mg/dm³. Due to this reason BDE cannot directly be discharged into the stream without proper treatment. The BDE is further treated aerobically to reduce COD and BOD, efficiency of which goes maximum up to 80%, and it is far away from the effluent discharge standard of central pollution control board (CPCB). Generally they prefer COD value of 250 mg/dm³ and BOD value of 30 mg/dm³ for the industries discharge in sewers⁵. Hence removal of COD and colour are necessary from BDE.

Various physicochemical treatment methods like wet oxidation^{6,7}, thermolysis^{8,9}, adsorption¹⁰ have been reported for the treatment of SW and BDE. These processes have several drawbacks. Thermolysis and wet oxidation process need rigorous operating condition and also it is not cost intensive. Adsorption process does not give very effective results.

Prajapati *et al.*¹¹ have reported the potential of $CuSO_4 \cdot 5H_2O$, Alum, FeCl₃, AlCl₃, and FeSO₄ · 7H₂O as a coagulant to remove COD and colour from BDE of rice grain based alcohol distillery. They achieved 78, 85, 68, 88, and 91% COD and 80, 80.46, 73, 80,

and 81.8% colour reduction with alum, AlCl₃, FeSO₄.7H₂O, and CuSO₄·5H₂O at their optimum condition. The detailed literature report is presented in Table 1.

This paper deals with the use of various coagulants such as CaCO₃, CuNO₃ and Na₂SiO₃ for the removal of COD and color from the BDE of rice grain based alcohol distillery. The reduction in chloride, phosphate, sulphur, carbohydrate, protein has been also calculated at their optimum pH. Settling studies have been also conducted.

Experimental Section

Materials

The BDE was obtained from Chhattisgarh Distillery Ltd Kumhari, C.G. (India). The analysis of sample is presented in Table 2. Laboratory grade reagent (L.R.) CaCO₃, CuNO₃ and Na₂SiO₃ were obtained from Merck India Ltd,, Mumbai (India). Whatman filter paper was supplied by GE Healthcare Ltd, Buckinghamshire (U.K).

Experimental method

BDE (0.5 dm³⁾ was taken in a 1 dm³ glass beaker. A known amount of coagulant was added to the effluent and mixed with the help of glass stirrer. The *p*H of effluent was noted and initial *p*H (*p*H_i) was adjusted by adding aqueous NaOH (2M) or H₂SO₄ (2M) solution and kept on jar test apparatus for coagulation process. The coagulant added BDE was

mixed for 15 min with the help of paddle stirrer at 100 rpm, after this it was slowly mixed (40 rpm) for 5 min. After the mixing process was complete the glass beaker was kept quiescent for about 4 h. Later on the supernatant liquor was filtered by Whatman filter paper (no 41) and its COD and colour value was analyzed. The steps were repeated for different

| Table 2 — Typical composition of biodigester effluent and the coagulant treated BDE | | | | |
|---|-------------------------|------------------------------|------------------------------|----------------|
| Parameters | Biodigester effluent | CuNO ₃ (40 mM) | CaCO ₃ (60 mM) | NaSi (40Mm) |
| COD | 11500 | 1955 | 2530 | 5635 |
| TDS | 43245 | 12964 | 14198 | 16738 |
| TSS | 39331 | 14039 | 15513 | 17160 |
| TS | 82576 | 27003 | 29711 | 33898 |
| Reduced carbohydrate | 517 | - | - | - |
| Protein | 165 | 105.2 | 113.5 | 120.3 |
| Chlorine | 161 | 106.8 | 112.1 | 117.4 |
| Phosphate | 0.05 | 0.15 | 0.1 | 0.35 |
| Total hardness | 10220 | 4130 | 1744 | 1612 |
| Sulphate | 4718 | 2312 | 2509 | 2704 |
| pH | 7.8 | 6.5 | 2.5 | 4.5 |
| Colour | Blackish brown | Greenish yellow | White | light brown |
| Absorbence at λ =475 nm | 0.831 | 0.1828 | 0.2077 | 0.4903 |
| Colour (PCU) | 398 | 87.56 | 99.5 | 234.82 |
| *All value in mg/dm ³ except pH, absorbance and colour | | | | |

*All value in mg/dm³ except pH, absorbance and colour

| | Table 1 — Characteristic of DWW | and the coagulation/flocculation treated ef | fluent | |
|--------------------------|--------------------------------------|--|-------------------|------------------|
| Investigator | Substrate | Coagulant | % COD/TOC removal | % Colour removal |
| Migo et al. (1993) | Molasses based | Polyferric hydroxysulphate (PFS) | | |
| | SW | | 21 | 32 |
| | BDE | | 73 | 87 |
| | LE | | 73 | 94 |
| | (TOC Removal) | | | |
| Chaudhari et al. (2005) | Molasses based BDECOD= 34000 | Poly aluminum chloride (PAC) | 72.5% | 92 |
| | | Aluminum chloride (AlCl ₃) | 60% | 86 |
| Prasad (2009) | Molasses based diluted SW | Ferric chloride (FeCl ₃) | 55% | 83 |
| | | | NR | 67 |
| | COD = 10000 - 11000 | MOC | | |
| Prajapati et al. (2014) | Rice grain based | | 91 | 81.8 |
| | BDE COD=13,600 | | 68 | 73 |
| | | Coppr sulphate (CuSO ₄) | 78 | 80 |
| | | Aluminum chloride (AlCl ₃) Ferric chloride (FeCl ₃) | 85 | 80 |
| | | Alum Ferric sulfate (FeSO ₄) | 85 | 80.64 |
| Note: All values observe | ed in optimum condition, COD in mg/c | dm ³ | | |

coagulant dosages. Settling study was performed in 0.5 dm^3 measuring cylinder.

Analytical procedure

The COD of the sample was determined by the close reflux method¹². Sulphate and phosphate contents were determined by standard methods¹². Protein was estimated by Lowry method¹³. Strength of the chlorine in sample was determined by standard titrametric method¹⁴. The reduced carbohydrate was estimated by Fehling method¹⁵. *p*H of sample was determined by using digital *p*H meter (EI Make, India). The colour of the samples were measured in terms of the absorbance at λ =475 nm using UV-spectrophotometer (Thermo Fisher, Germany)¹⁶.

Results and Discussion

The characteristic of BDE shows (Table 2) reduced carbohydrate, melanoidin and proteins. The presence of similar components have been reported in molasses based SW and BDE, but they differ in their quantities¹⁷. Carbohydrates provide carboxylic and hydroxyl functional groups. Lignin is in very little amount in rice grain based BDE. Protein structured by amino acid, which after the neutralization provide negative charge. Melanoidin also posses net negative charge¹⁶. The BDE contain more colloidal particles than SW, therefore BDE treatment is better option to treat SW by coagulation process¹¹. The colloidal surfaces have negative charge. In the experiments coagulants like CaCO₃, CuNO₃, and Na₂SiO₃ were used to treat BDE. When CaCO₃ was added in BDE it released Ca⁺ ions, similarly Na₂SiO₃ released Na⁺ ions, which gets attached to the negative ions of BDE. Coagulant ions undergo hydrolysis and generate several monomeric and polymeric species.

Copper nitrate releases number of Cu²⁺ ions. It also forms monomeric and polymeric species. The metal hydroxide polymers have been found to possess positive charge amorphous structure with large surface area and are hydrophobic in nature¹⁸. As they are hydrophobic in nature it adsorbs and neutralizes the organic anionic particles which settle down due to its heavy mass, further promoting sweep coagulation¹⁹. The anhydride metals remains in the cation form also tends to associate with a number of functional groups of organic components contained in wastewater. The negative charges of these functional groups are neutralized by it, resulting in colloidal destabilization and precipitation of the metal (cations) -organic (anions) complex. When the complex settles down due to gravity it also adsorbs the contaminants (organic and inorganic amorphous flock) along with it. Amorphous $M(OH)_3$ flocs are also formed, which have large surface area that helps in rapid adsorption of soluble organic compounds and trapping of colloidal particles. These flocs are removed by sedimentation. The general form of hydrolysis reaction of trivalent metals is given as¹⁶:

Aqueous solution

| Coagulants => | Compound | cations | + | Anions | $(CO_{3}^{-},$ |
|------------------------|----------|---------|---|--------|----------------|
| NO_3^- , SO_4 etc) | | | | | (1) |

$$xM^{3+} + yH_2O \rightarrow Mx(OH)y^{(3x-y)+} + yH^+$$
 ... (2)

Effect of pH

The initial *p*H has been found to have tremendous effect on coagulation process; therefore, the COD and colour reduction of BDE with coagulant calcium carbonate at different *p*H were studied with *p*H variation from *p*H 1.5 to 10.5. It was found that 75, 78, 60, 66, 69 and 62% COD reduction and 67, 75, 52, 61, 63 and 56% colour reduction were achieved at *p*H 1.5, 2.5, 4.5, 6.5, 8.5 and 10.5 and are presented in Fig. 1 and Fig. 2. Copper nitrate is an important coagulant to treat BDE. After treatment results showed 58, 66, 83, 71 and 67% COD reduction and 51, 59, 78, 67 and 63%, colour reduction at *p*H 2.5, 4.5, 6.5, 8.5 and 10.5. Any variation from *p*H 6.5, the COD and colour removal efficiency was reduced.

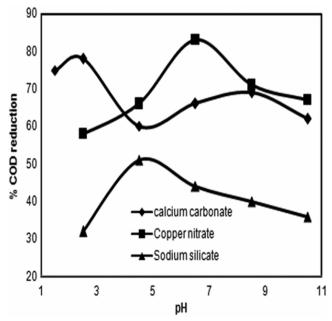


Fig. 1 — Effect of pH_i COD reduction of BDE using different coagulants. CaCO₃ = 60 mM, CuNO₃ = 40 mM, NaSi = 40 mM

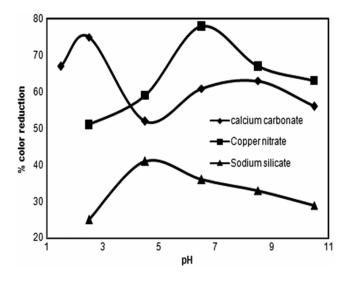


Fig. 2 — Effect of pH_i on colour reduction of BDE using different coagulants. CaCO₃ = 60 mM, CuNO₃ = 40 mM, NaSi = 40 mM

Decreasing trend of COD reduction was observed for pHi < 2.5 and 6.5< pHi <6.5. Further increase in pHi showed increase in COD reduction. Na₂SiO₃ was also used to treat BDE, COD reduction of 32, 51, 44, 40, 36% and color reduction of 25, 41, 36, 33and 29% with 40 mM coagulant dose and at pH 2.5, 4.5, 6.5, 8.5 and 10.5 was achieved. It was seen that COD and colour reduction of the BDE is function of pH. This may be due to the reaction rate of coagulant cations depending on the number of H⁺ ions generated during the process.

The decolorization is expressed as the percent decrease in the absorbance of the treated BDE sample from the untreated sample at $\lambda = 475 \text{ nm}^{12}$. The decolorization is due to removal of melanoidin and other organic components which separates out from the effluent during coagulation.

The formation of compound hydroxide cations are governed by the *p*H of the solution. The quantity and quality of these species contributes the two mechanisms of coagulation charge neutralization and sweep flocculation. Charges on functional groups present in the effluent also vary with *p*H. For the CaCO₃, CuNO₃ and Na₂SiO₃ the optimum *p*H was 2.5, 5 and 4.5 respectively. At the optimum *p*H and coagulant dosages, COD reductions are less as compared to the colour reductions, because some amount of organic matter were still present in treated water which enhances the COD value.

Effect of coagulant dosages

To get optimum dosage for different coagulants on basis of COD reduction and colour reduction of BDE,

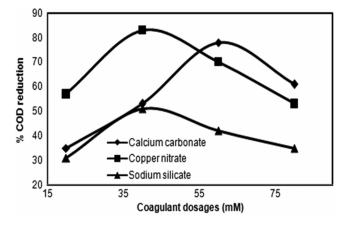


Fig. 3 — Effect of coagulant doze on (a) COD reduction BDE at optimum *p*H using different coagulants. $COD_i=11500 \text{ mg/dm}^3$. $CaCO_3 = pH 2.5$, $CuNO_3 = pH 6.5$, NaSi = pH 4.5

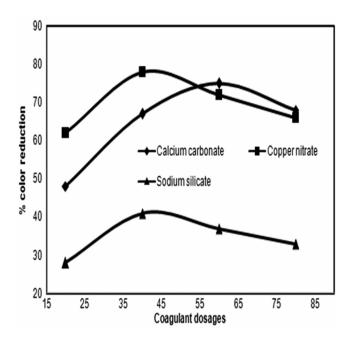


Fig. 4 — Effect of coagulant doze on colour reduction of BDE at optimum *p*H using different coagulants. $COD_i=11500 \text{ mg/dm}^3$, colour_i = 430 PCU. $CaCO_3 = pH 2.5$, $CuNO_3 = pH 6.5$, NaSi = pH 4.5

different dosage of CaCO₃, CuNO₃ and Na₂SiO₃ was used during the experiments. The results are presented in Fig. 3 and Fig. 4. The effect of CaCO₃ on COD and colour reduction was studied with different coagulants dosages at their optimum *p*H. COD reduction of 35, 53, 78, and 61% and colour reduction of 48, 67, 75 and 68% was achieved, with coagulant dosages of 20, 40, 60 and 80 mM CaCO₃.

While using copper nitrate, 57, 83, 70 and 53% COD reduction and 62, 78, 72 and 66% colour reduction with coagulant dosages 20, 40, 60 and 80 mM was achieved. It was observed that any

variation from coagulant dosage of 40 mM the COD and colour removal efficiency reduced. Decreasing trend of COD reduction was observed for coagulant dosage of 40 mM \leq coagulant dosage \leq 40 mM.

Na2SiO3 showed very poor result and 31, 51, 42, 35 COD reduction and 28, 41, 37, and 33% colour reduction with 40 mM coagulant dosage at the optimum pH was achieved.

The increase in coagulant dosages up to certain limit results in formation of more compound cations, compound hydroxide cations and also may be more neutralized compound hydroxide. These resulted in the increase in COD and colour reduction. The high dosages of coagulants destabilize and neutralize the organic anions thereby causing for higher colour intensity.

The effect of coagulant dosage on variation of original *p*H of BDE is shown in Fig. 5. The original *p*H value of the BDE was 7.8 which changed with the addition of coagulants. Coagulants CaCO₃ showed neutral characteristic, CuNO₃ showed acidic nature and Na₂SiO₃ showed alkaline nature. When 20 mM CaCO₃ was added in BDE, the *p*H value reduced to 7.2. Further addition of CaCO₃ in the BDE, the *p*H remained nearly the same. Similarly 20 mM CuNO₃ reduces the *p*H value of BDE to 4.46 and further increasing the coagulant dosages upto 80 mM the *p*H remains constant. However 20 mM Na₂SiO₃ increases the *p*H value of BDE to 9.38 which increases up to *p*H 12.62 with coagulant dosages of 80 mM.

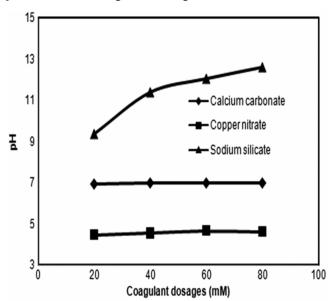


Fig. 5 — Effect of coagulant doze on the variation of pH of BDE. pH_{i} =8.0

Settling study of the treated effluent

It is necessary to separate the sludge and liquid contents of slurry mixture in sedimentation apparatus. Sedimentation is the most economic method compared to the other separation processes. To study the separation characteristic by settling, the BDE after coagulation process was slowly mixed and taken in 0.5 dm³ cylinder having diameter 4.6 cm. The supernatant and solid interphase was noted with time. Figure. 6 shows the time Vs height graph of settling sludge of different coagulants. It was observed that the settling of the solids is faster initially and after some time, it decreases. The portion in which settling is faster is known as zone settling region and the portion where a compressed layer begins to form at the bottom of the cylinder is called compression settling region. The settling rate was found in the order of CaCO₃> CuNO₃> Na₂SiO₃>. CaCO₃ showed better settling but poor COD and color reduction as compared to other coagulant. Several methods have been presented for the evaluation of compression zone depth. Using the batch sedimentation data a continuous thickener may be designed²⁰. Method proposed by Richardson *et al.*²⁰ is common to design a continuous thickener based on batch studies.

Analysis of filtrate

The filtrate was analyzed before and after the treatment of BDE, the result is presented in Table 2. It was observed that large amount of COD was reduced after coagulation/ flocculation process (83% COD reduction using CuNO₃). The colour was also reduced up to 78%. Soluble lignin was absent in BDE.

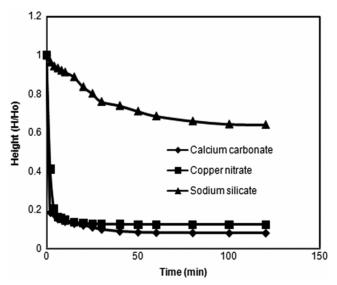


Fig. 6 — Settling characteristic of the coagulated slurry.

| Table 3 — Analysis of residue obtained after coagulation | | | | |
|--|------------------------------|------------------------------|----------------|--|
| Coagulant | CuNO ₃ (40 mM) | CaCO ₃ (60 mM) | NaSi (40Mm) | |
| Initial $pH(pH_0)$ | 5 | 5 | 6 | |
| Weight of residue | 30.31 | 15.78 | 14.15 | |
| (kg/m^3) | | | | |
| Colour | Brown | Dark brown | Dark brown | |
| Nature | Bulky mass, | Bulky mass, | Bulky mass, | |
| | difficult to | difficult to | difficult to | |
| | grinding | grinding | grinding | |
| Approximated | 13 | 10 | 8 | |
| drying period | | | | |
| % Convertible COD | 83 | 78 | 41 | |

Reduced carbohydrate, proteins, chloride, phosphate, sulphate, total hardness and total solid were also reduced up to a satisfactory level from the BDE. Table 1 also shows that after treatment many functional group and chemicals (organic and inorganic) were reduced from the BDE. CuNO₃ gave better result (83% COD and 78% colour reduction) as compared to the other coagulant like Na₂SiO₃ and $CaCO_3$. The result shows that the COD (1955-5635 mg/L) and color level does not conform to the dischargeable limit for the treated BDE. The central pollution control board (CPCB), India has norms that the COD of BDE should not greater than 250 mg/dm³. Hence, further treatment of coagulated treated BDE is necessary. The wet oxidation, membrane separation processes are possible alternate to treat it further so as to reach the dischargeable limit.

Analysis of residue

After the separation of solid residues from the treated BDE, it was further characterized. Residues of different coagulant were dried at 115° C and then analyzed. The data of analysis is presented in Table 3. It was found that the weight of CuNO₃ treated residue was highest. Color and approximated drying period was different for different sludge. The nature of the residues were found to be hard and difficult to grind. It has been reported that these organic residues have good heating value²¹⁻²³.

Conclusion

Coagulation/flocculation process for treatment of BDE of a rice grain-based distillery is an effective treatment method to reduce its COD and colour. CuNO₃, CaCO₃ and Na₂SiO₃ gave 83, 78 and 51% COD reduction and 78, 75 and 41% color reduction at their optimum *p*H 6.5, 2.5 and 4.5 respectively. The *p*H of the BDE plays a very significant role. The COD and color reduction was found to increase considerably

with the increase in the dosages of coagulants up to certain limit (up to 40-60 mM). Reduction of COD was not found by further increase in coagulant dosage.

The settling characteristic of $CaCO_3$ treated BDE was found to be best among effluents treated with CuNO₃ and Na₂SiO₃. Flirtation studied showed treated BDE does have good filterability. Complete removal of COD and BOD from the BDE was not possible by coagulation/ flocculation method. Thus further treatment by using aeration, wet oxidation, and membrane separation can be undertaken.

References

- 1 Berg C, *World fuel ethanol analysis an outlook*, 2004. www.distill.com (accessed on 10.02.2008).
- 2 Lele S S, Shirgaonkar I J & Joshi J B, *Indian Chem Eng*, 32 (1990) 36.
- 3 Belkacemi K, Larachi F, Hamoudi S, Turcotte G & Sayari A, Ind Eng Chem Res, 38 (1999) 2268
- 4 Wolmarans B, Gideon H & Villiers D, Water SA, 28 (2002) 63.
- 5 Indian standard specification IS: 271 (Bureau of Indian Standard, New Delhi) 1975.
- 6 Belkacemi K, Larachi F, Hamoudi S & Shayari A, *App Cataly A: G*, 199 (2000) 199.
- 7 Dhale A D & Mahajani V V, Indian J Chem Tech, 7 (2000) 11.
- 8 Chaudhari P K, Chand S & Mishra I M, *Chem Engg Commn*, 199 (2012) 1.
- 9 Chudhari P K, Mishra I M & Chand S, *Ind Eng Chem Res*, 44 (2005) 5518.
- 10 Satyawali Y & Balakrishnan M, Bioresource Technol, 98 (2007) 2629.
- 11 Prajapati A, Choudhary R, Verma K, Chaudhari P & Dubey A, *Desalination Water Treat*, 2013, DOI: 10. 1080/19443994.2013. 86274.
- 12 Clesceri L, Greenberg A E & Trussell R R, Standard Methods for Water and Waste Water Examination, Vol. 1, 17th Edn (APHA, New York), 1989.
- 13 Larson E, Howlett B & Jagendorf A, Analy Biochem, 155 (1986) 243.
- 14 Vogel A I, A Text Book of Quantitative Inorganic Analysis, Vol. 1, 17th Edn (Longman, London), 1958, 208.
- 15 Mann F G & Saunders B C, Quantitative Analysis in Practical Organic Chemistry, Part IV Vol. 1, 4th Edn (Longman, London), 1960, 421.
- 16 Ching H W, Tanaka T S & Elimelech M, Water Res, 28 (1994) 559.
- 17 Chaudhari P K, Mishra I M & Chand S, Colloids Surf A: Physicochem Eng Asp, 296 (2007) 238.
- 18 Chaudhari P K, Majumdar B, Choudhary R, Yadav D K & Chand S, *Environ Tech*, 31 (2010) 357.
- 19 Peavey S & Rowe R, *Environmental Engineering*, Vol 1, 2nd Edn (McGraw-HILL International New York), 1985, 485.
- 20 Richardson J, Harker J & Backhurst J, Coulson and Richardson's Chemical Engineering
- 21 Particle Technology & Separation Processes, vol. 2, 2nd end (Elsevier India Pvt. Ltd. Chennai) 2003, 678.
- 22 Prajapati A & Chaudhari P, Chem Eng Technol, 37 (2014) 65.
- 23 Prajapati A & Chaudhari P, Environ Technol, 35 (2014) 242.
- 24 Kumar P, Prasad B, Mishra I M & Chand S, *J Hazard Mater*, 149 (2007) 26.